

IOWA STATE UNIVERSITY

Fatigue Properties of Steel Castings and their Relation to NDE Results

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Goals

- Analysis of castings via NDE and surface classification methods
- Determine the effect casting surface and near surface condition on fatigue life
- Develop relationship between NDE results and casting life

Test Plan

- Visually inspect per ASTM A802 (SCRATA)
- Laser scan
- Create rubber impressions of the surface
- Radiography
- Magnetic Particle Inspection
- Decide locations of test bars
- Water jet test bars from plates
- Uniaxial fatigue testing on test bars including areas of interest (surface and internal discontinuities)
- Material characterization by UAB

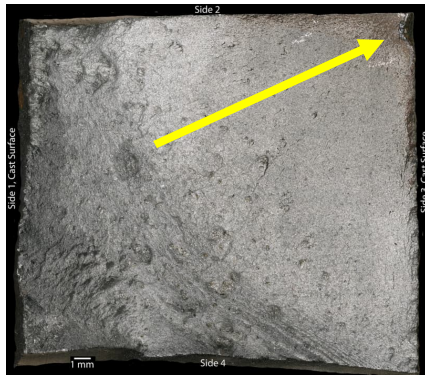
Initiation Site Examples from UAB Images

Casting/Side - Gas

Cycles:
1,099,616

Initiation site
length:
0.97mm

Variogram
avg:
0.061mm

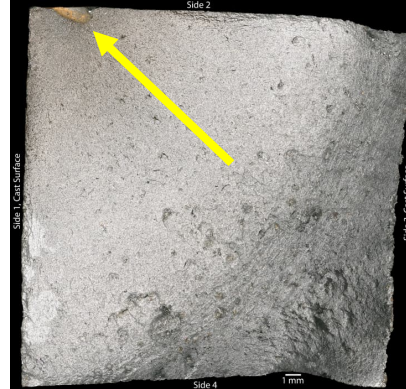


Cutting Gouges

Cycles:
2,794,392

Initiation site
length:
1.33mm

Variogram
avg:
0.061mm

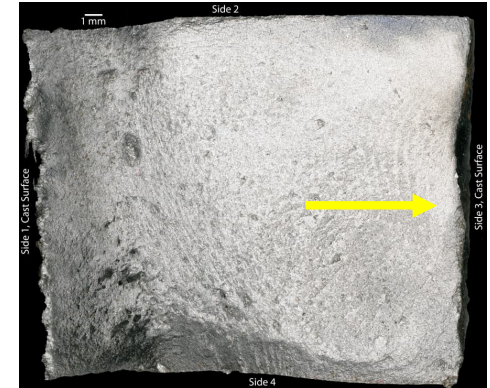


CS=Cast Surface

Cycles:
751,221

Initiation site
length:
N/A

Variogram
avg:
0.087mm

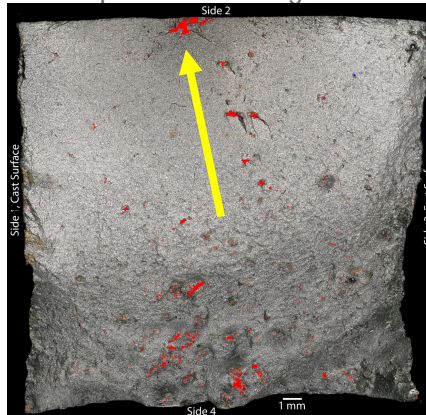


Exposed Shrinkage

Cycles:
425,687

Initiation site
length:
0.75mm

Variogram
avg:
0.075mm

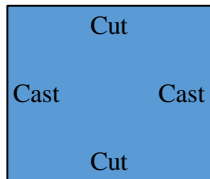
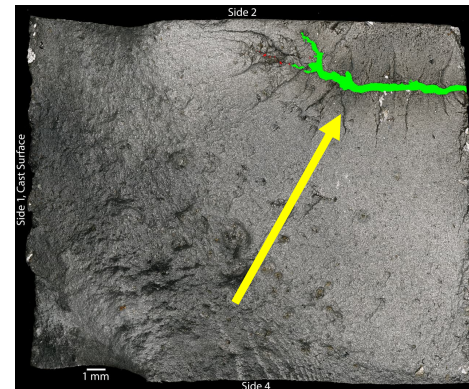


Gas

Cycles:
298,751

Initiation site
length:
2.05mm

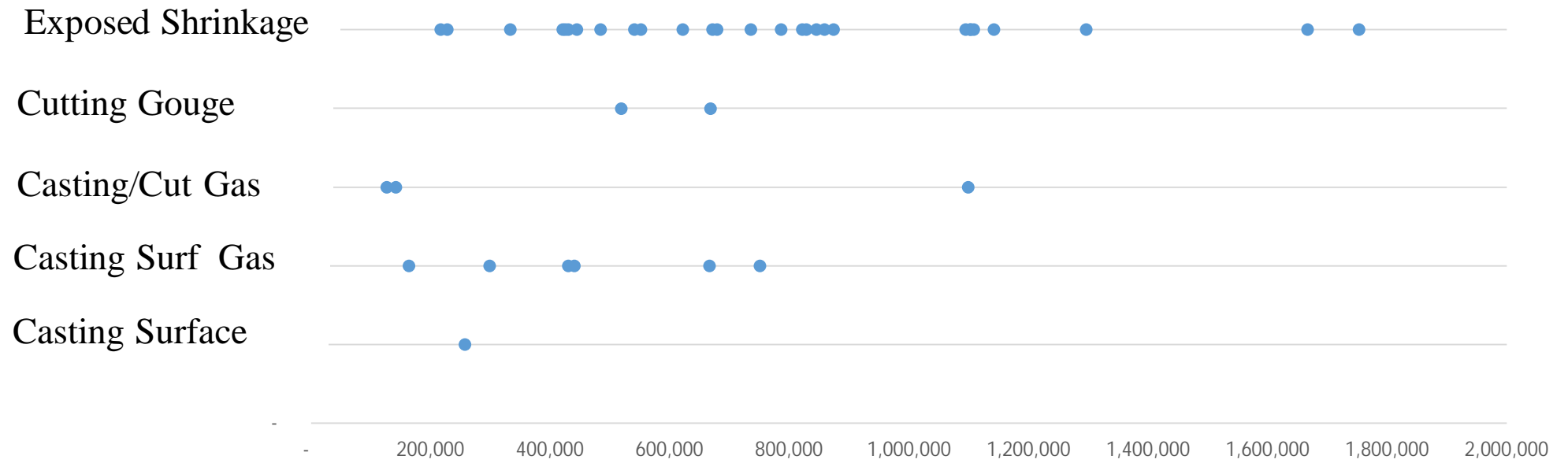
Variogram
avg:
0.08mm



WCB Testing Results – By Cause

Did Not Fail

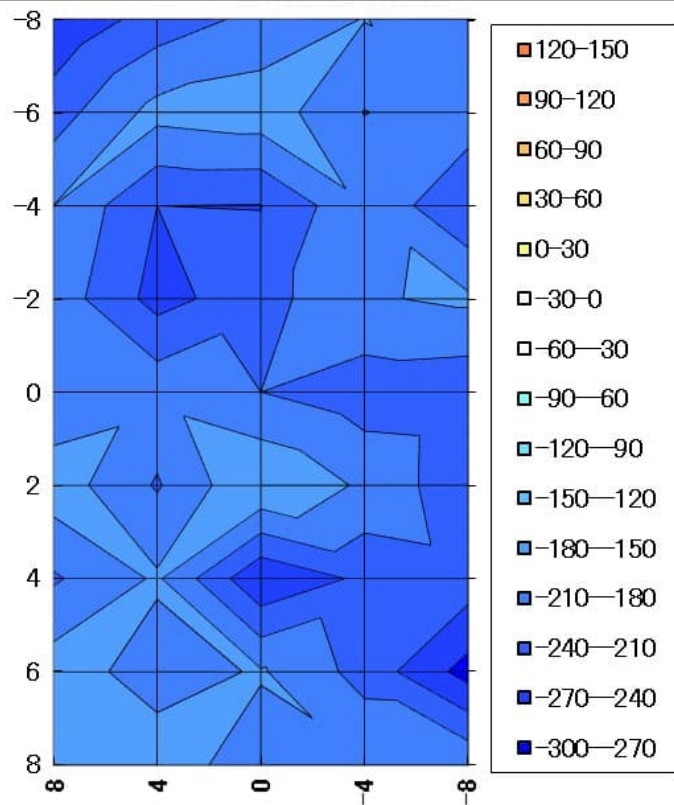
6 specimens



Sample "G1" Front

Min: -282 MPa

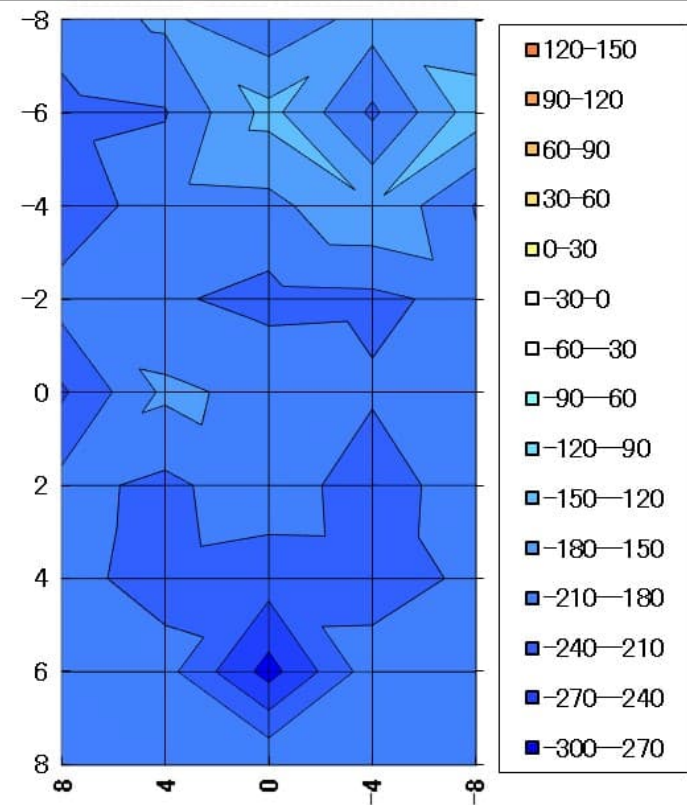
Max: -151 MPa

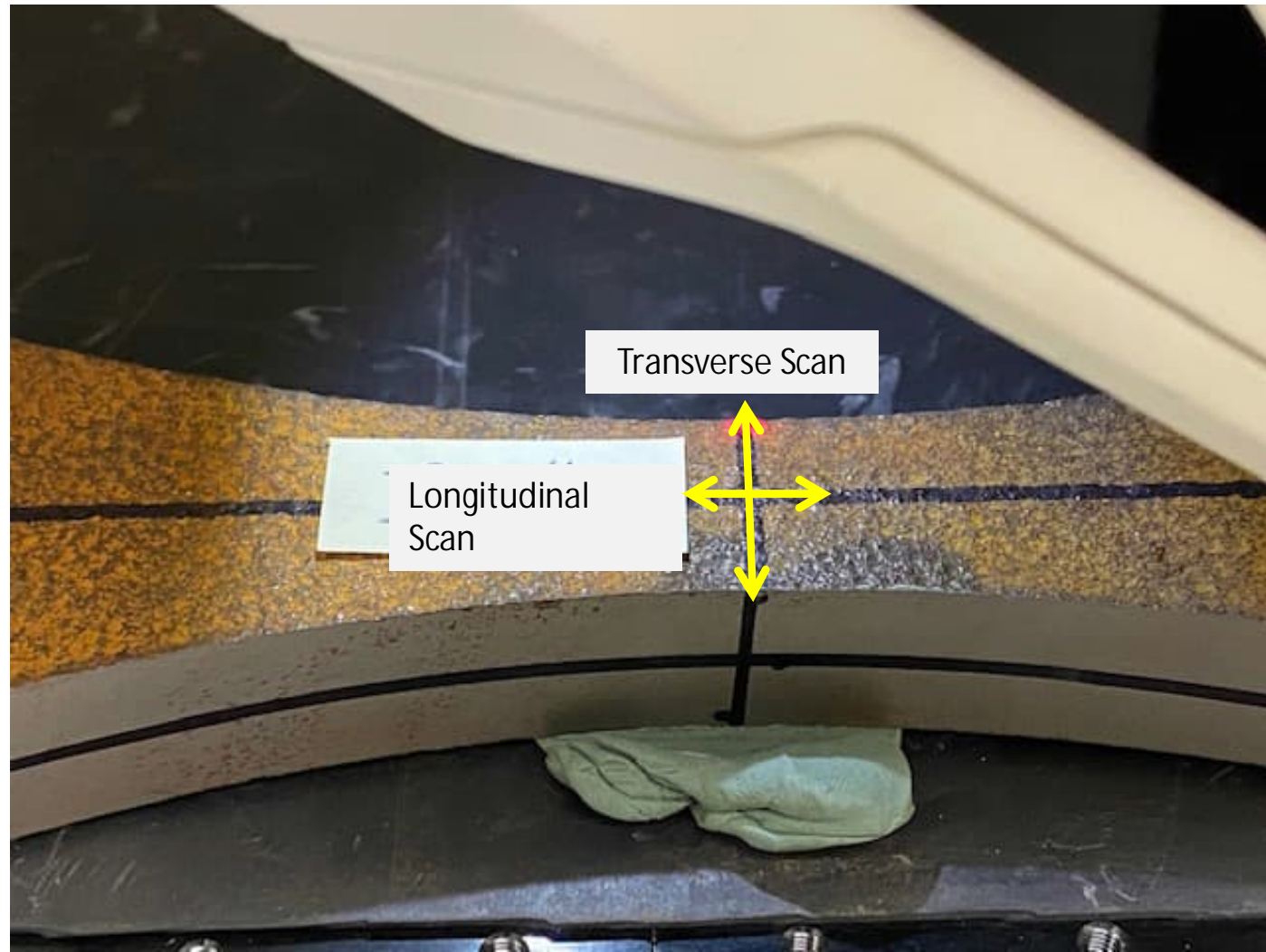


Sample "G1" Back

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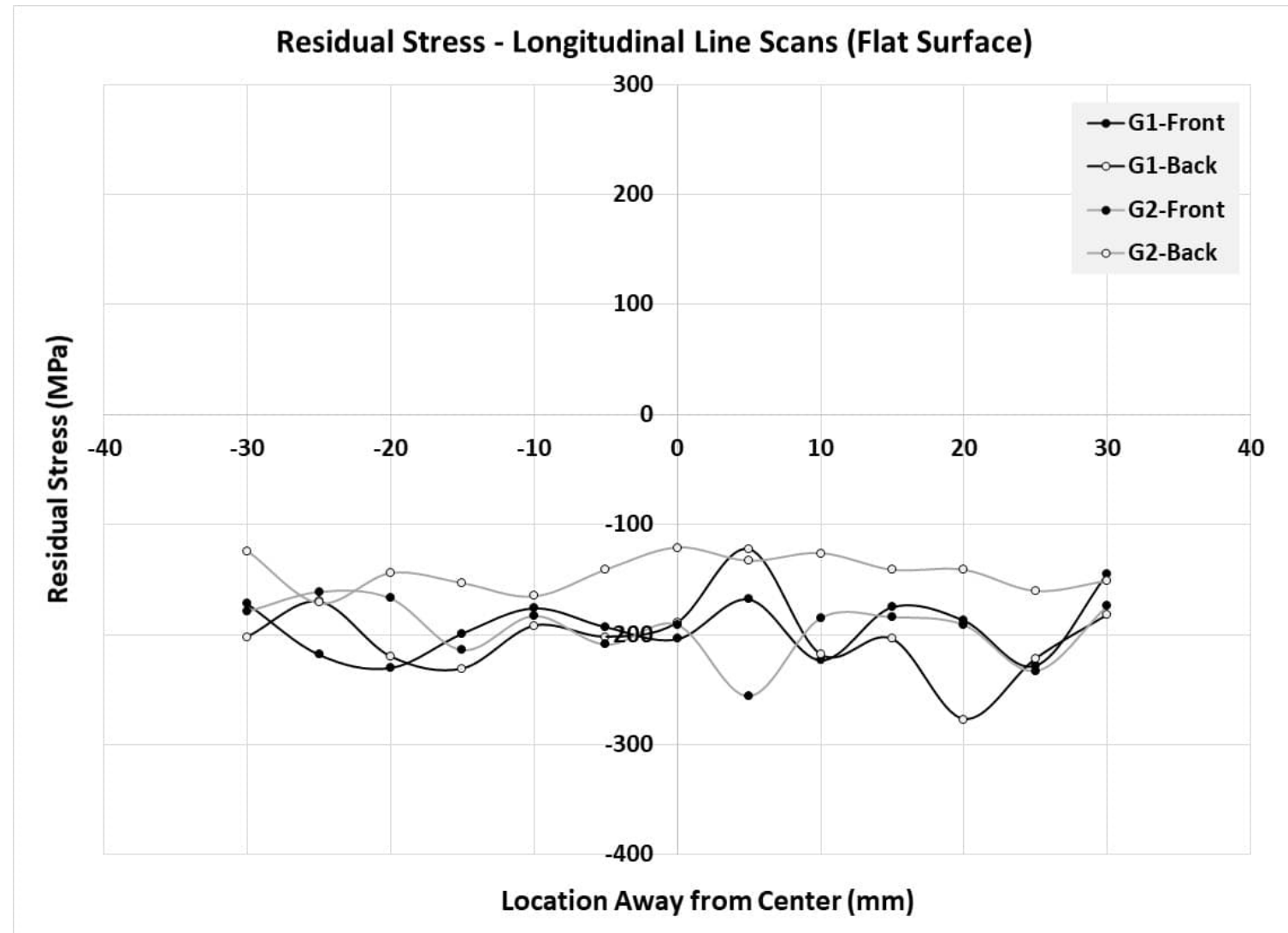
Max: -134 MPa





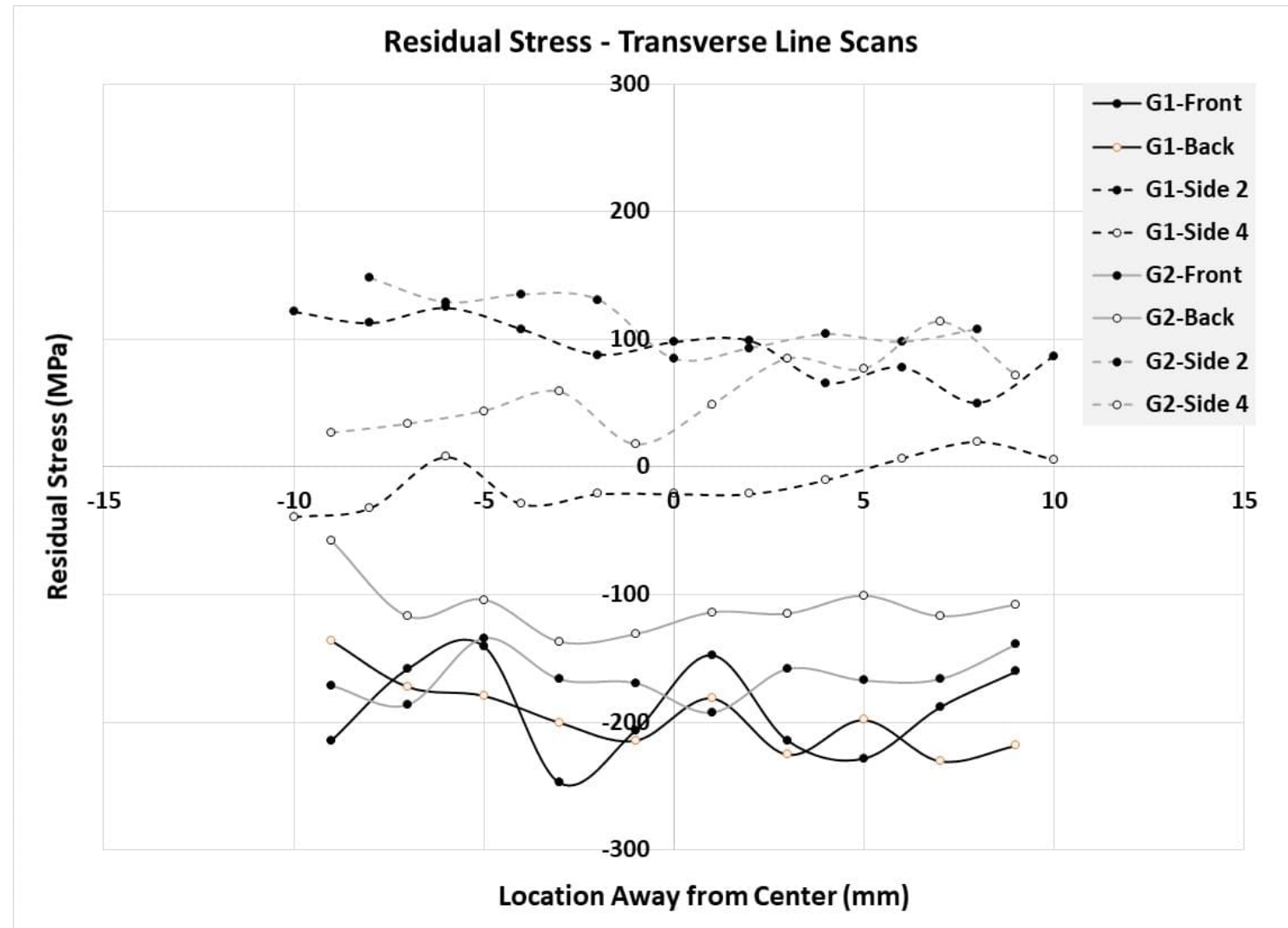
Longitudinal line scans, which were only possible on the flat as-cast surfaces

As-cast surfaces exhibited a lower (more compressive) residual stress. This is likely due to abrasive blast cleaning.



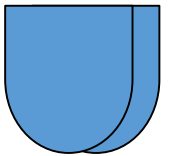
Transverse line scans, which were possible on all sides

Machined surfaces exhibited a higher (more tensile) residual stress



Moving Forward

- “Now exposed” center line shrinkage is dominating results
- Conduct testing of WCB specimens with EDM notches in gage length.
- Plate for 8630 plate with improved riser design



8630 Plates –





Plate #
114



Plate #
114
A B

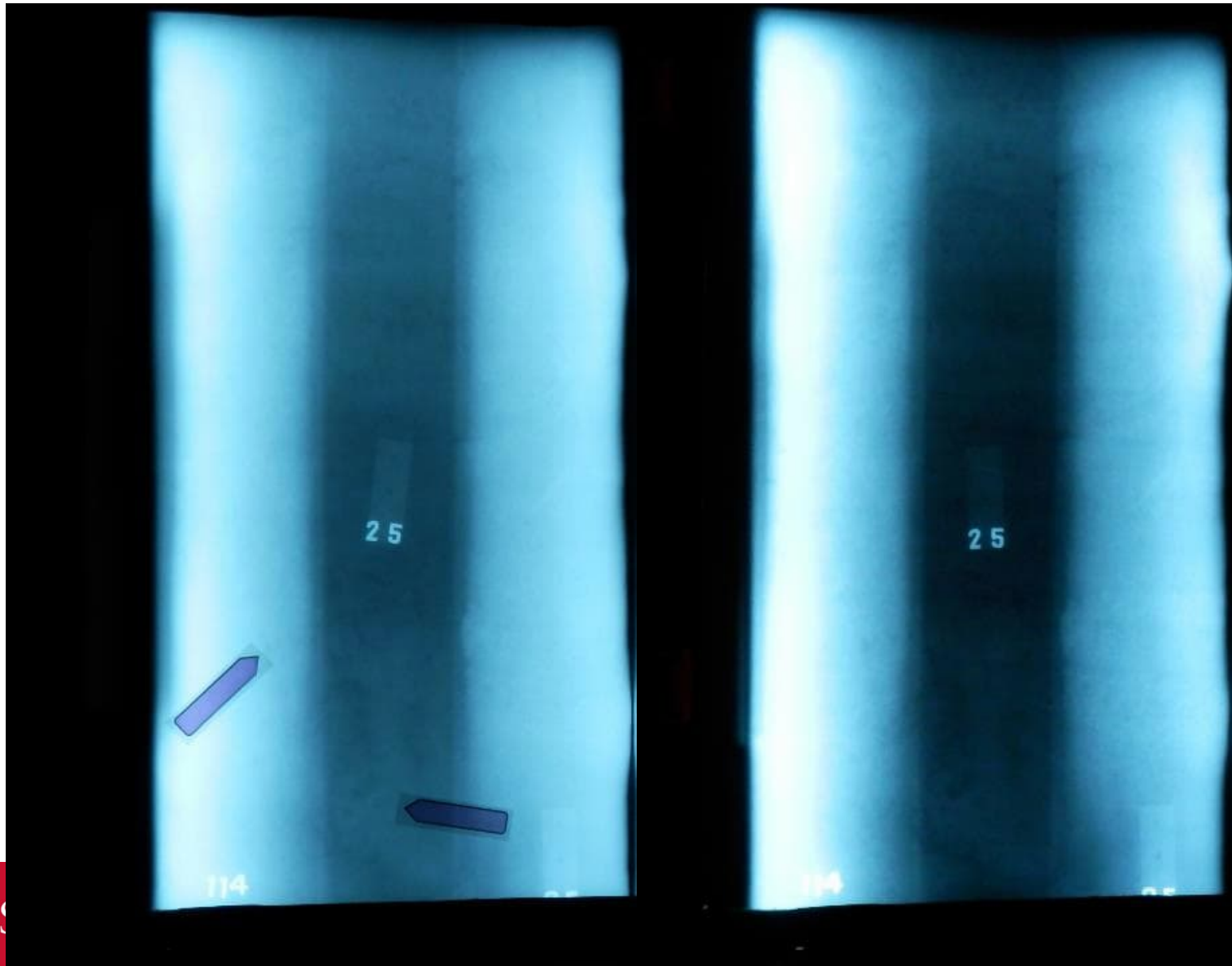
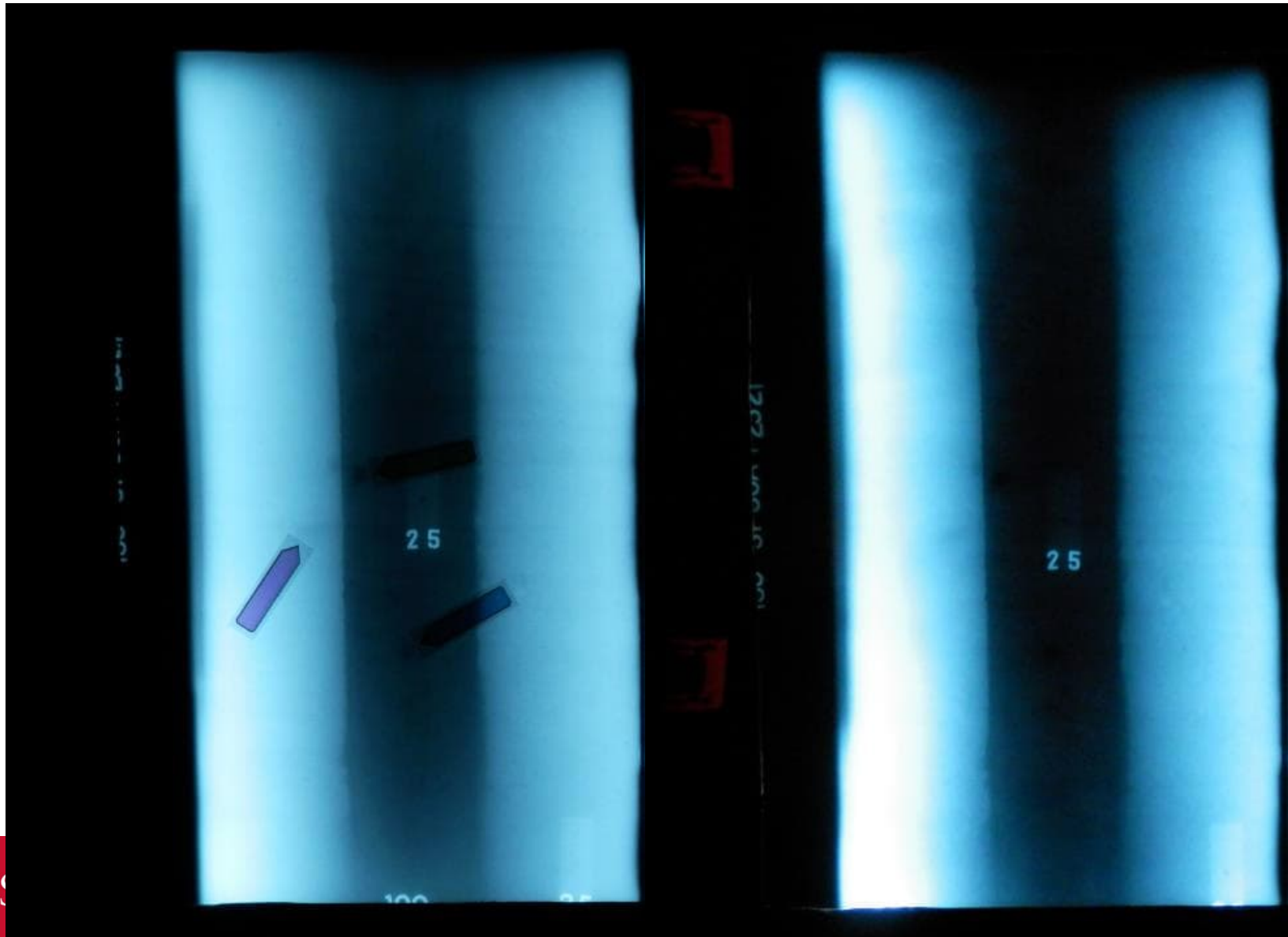


Plate #
100

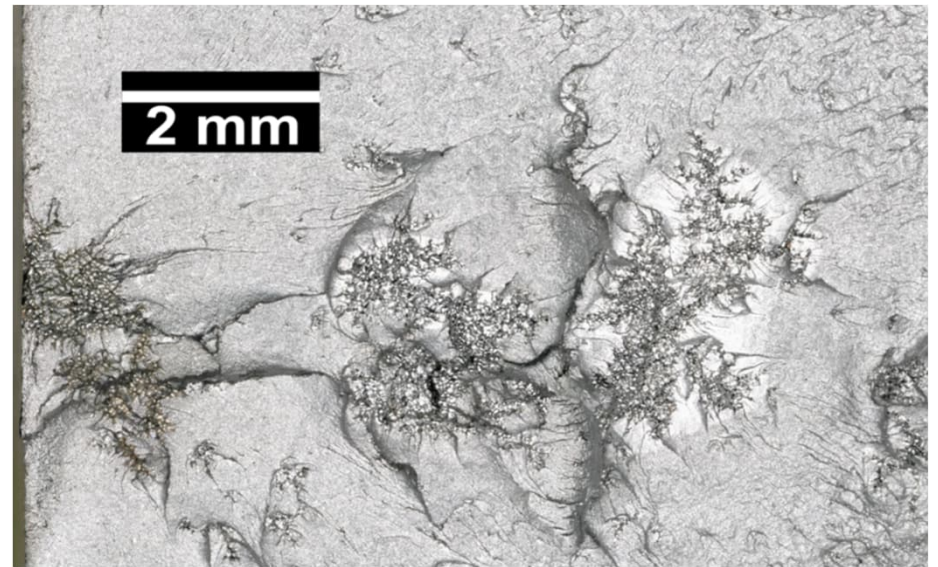
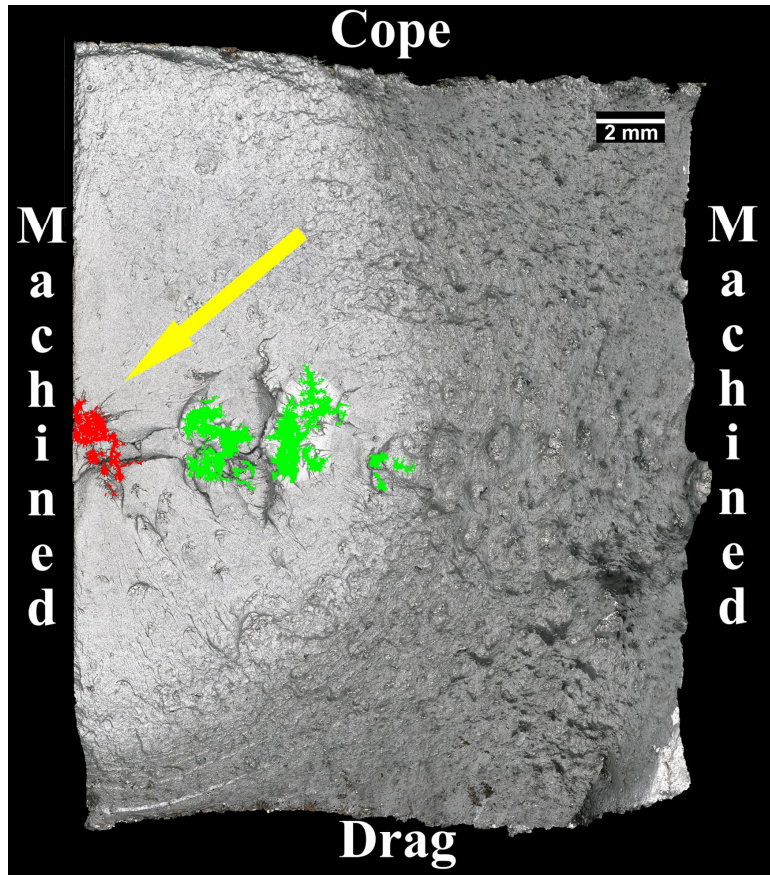


Plate #
100
A B





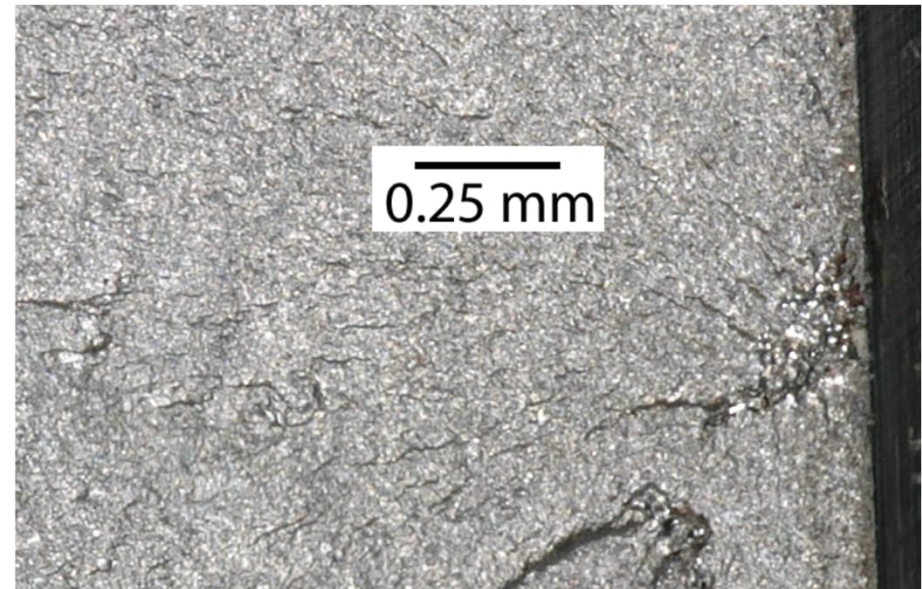
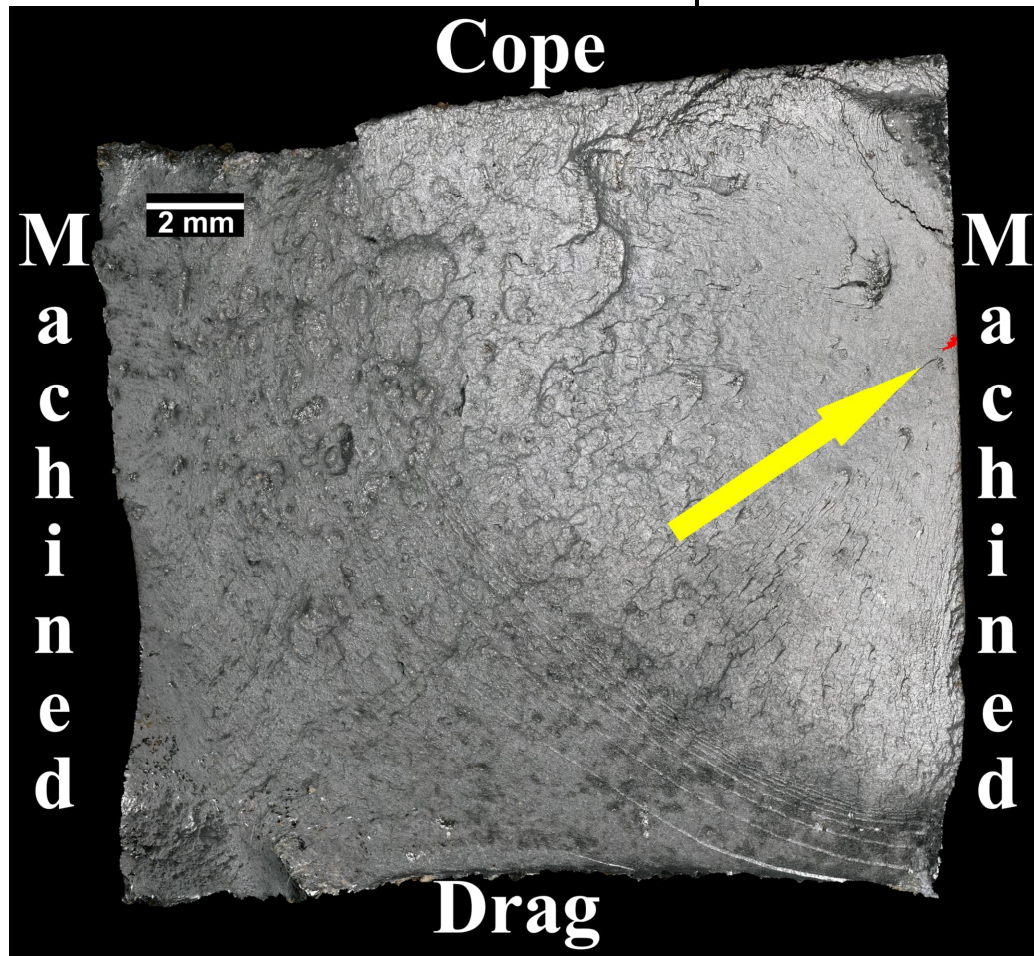
Set 5 Specimen 100-1



Zoom of Initiation Site

Yellow arrow points to initiation site
Red area is porosity at initiation site
Green area is porosity at secondary cracks

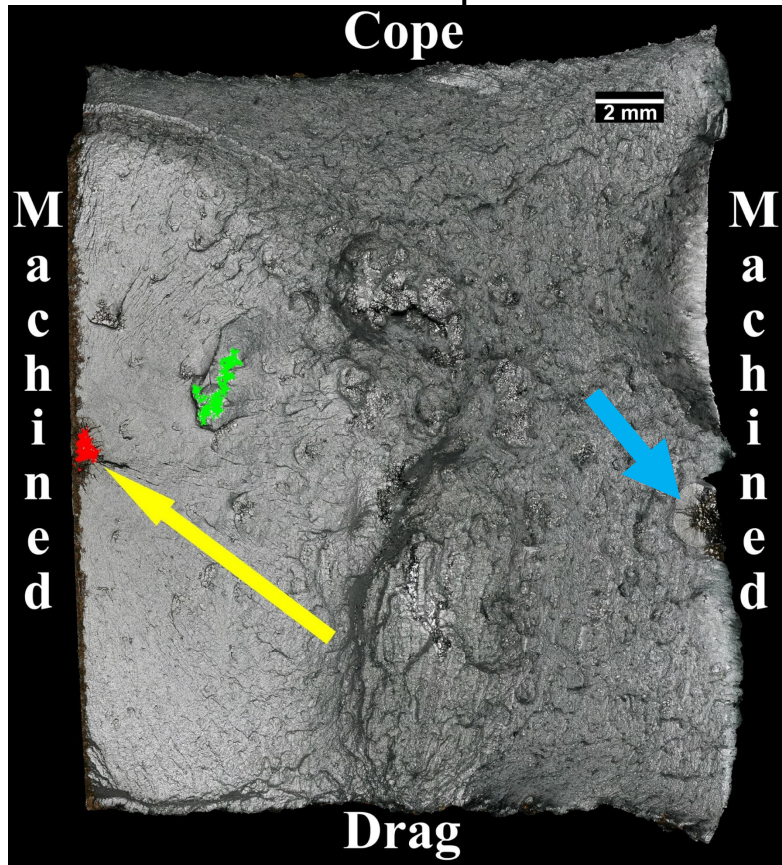
Set 5 Specimen 100-2 **MIDDLE BAR**



Yellow arrow points to initiation site
Red area is porosity at initiation site

Set 5 Specimen 100-3

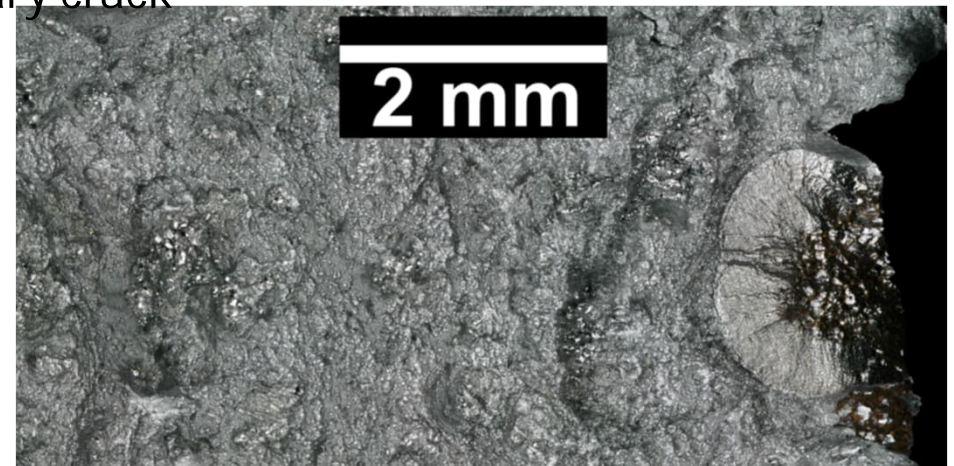
Cope



Blue arrow points to opened up secondary crack on machined surface opposite initiation side.

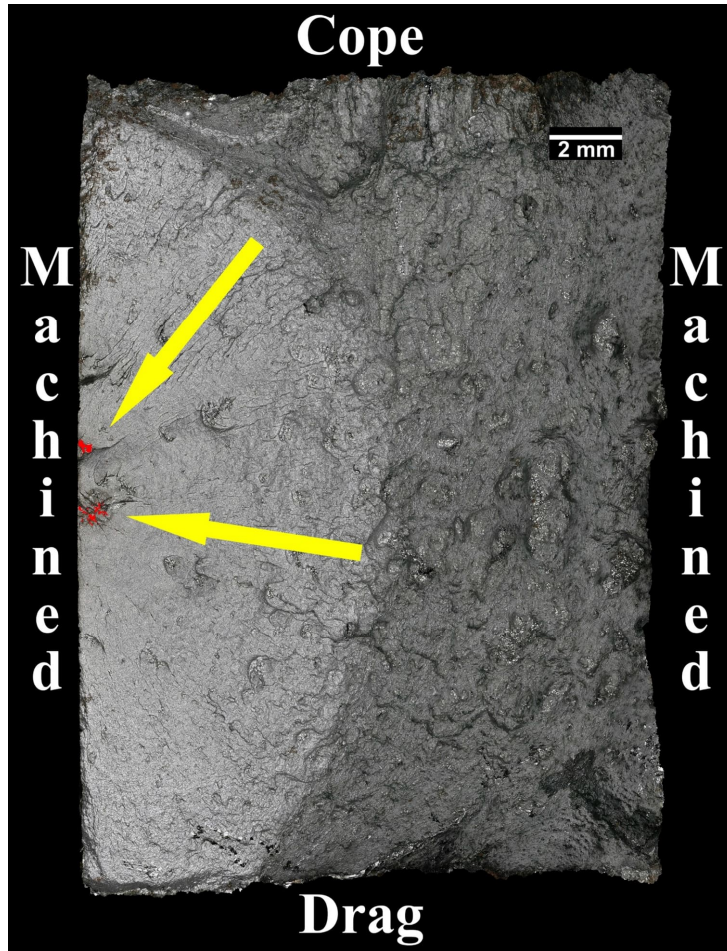


Machined surface opposite initiation side showing secondary crack

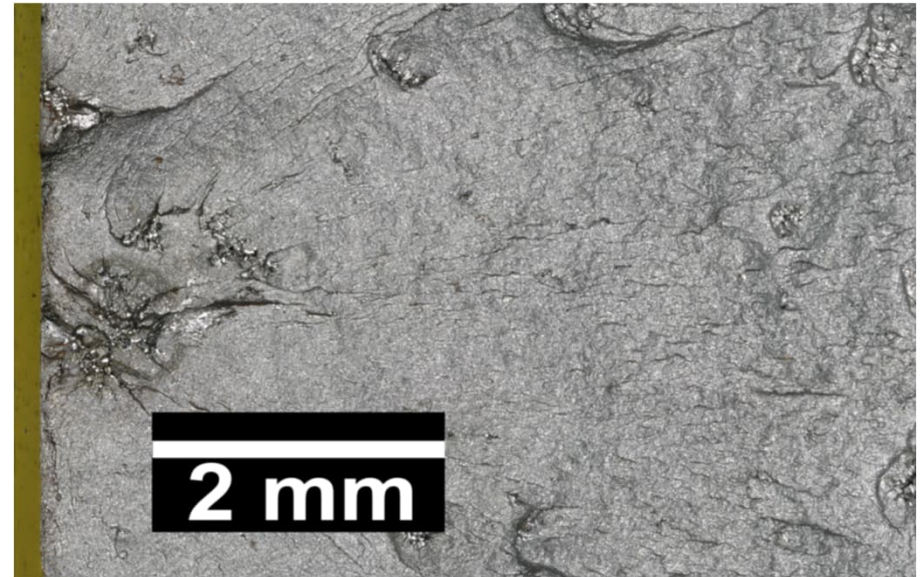


Zoom of opened-up secondary crack.

Set 5 Specimen 114-1

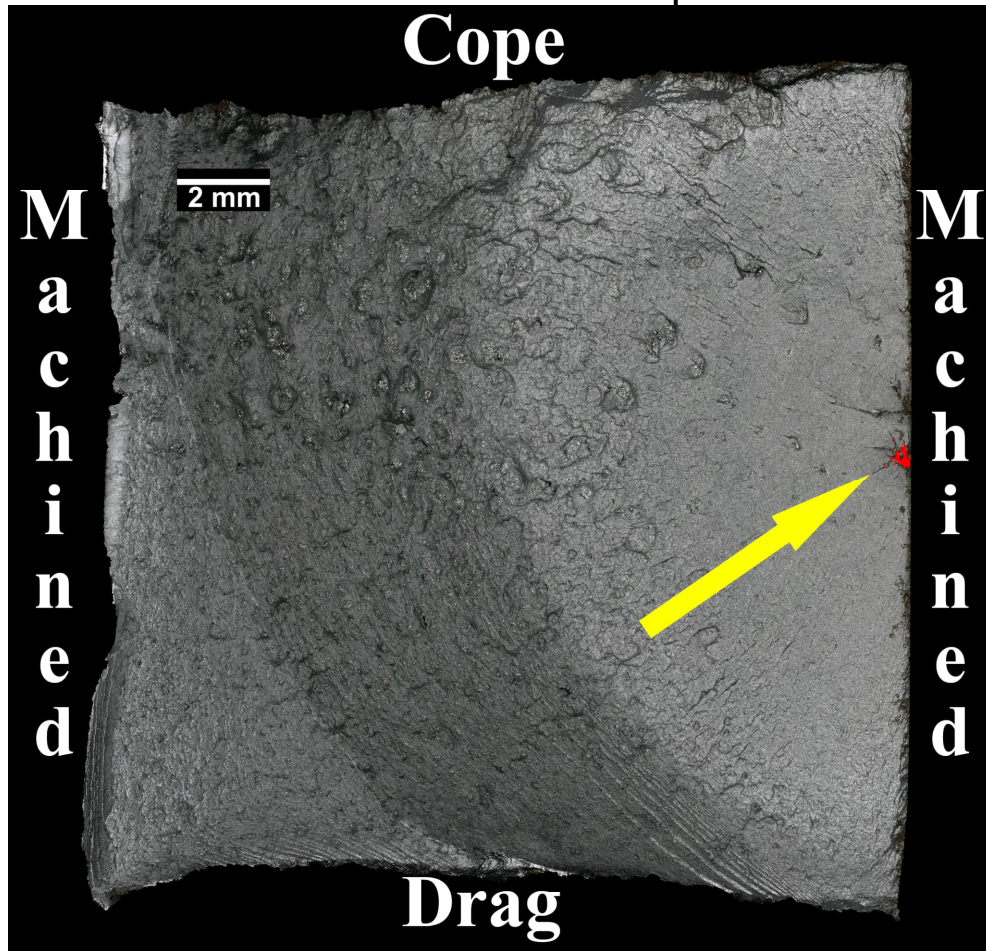


Yellow arrow points to initiation site
Red area is porosity at initiation site

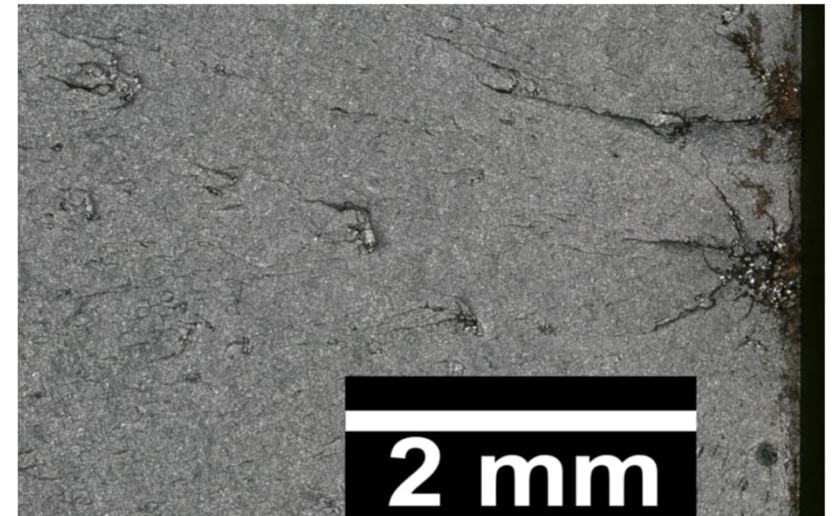


Zoom of initiation site

Set 5 Specimen 114-2 **MIDDLE BAR**

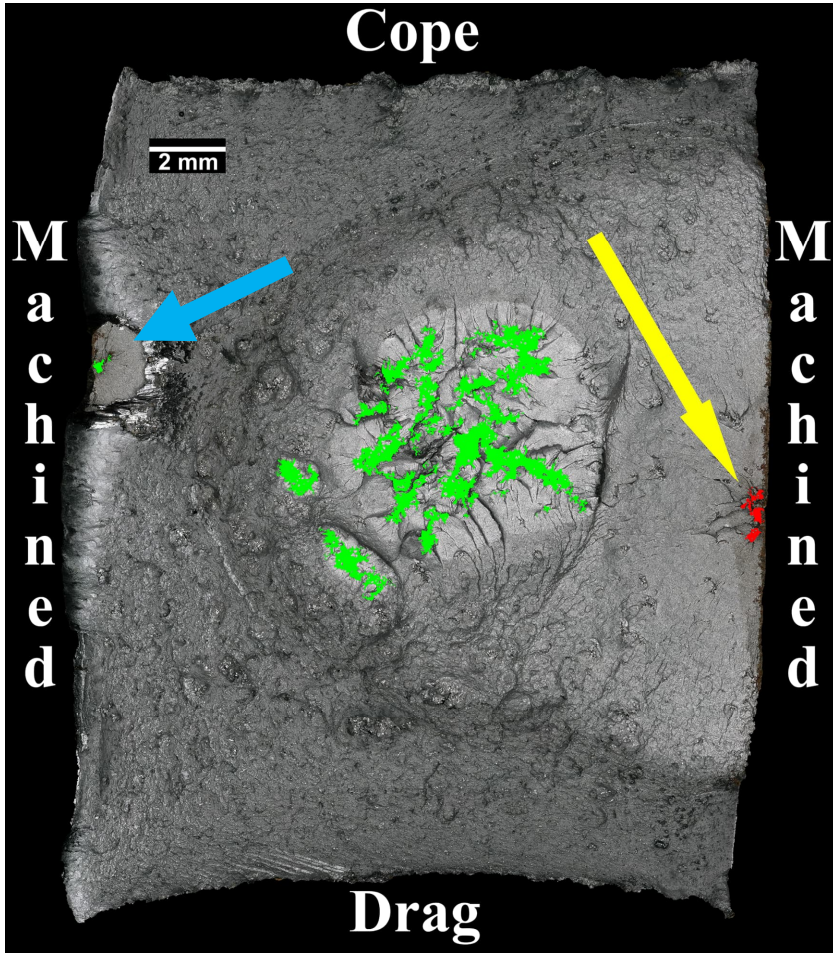


Yellow arrow points to initiation site
Red area is porosity at initiation site



Set 5 Specimen 114-3

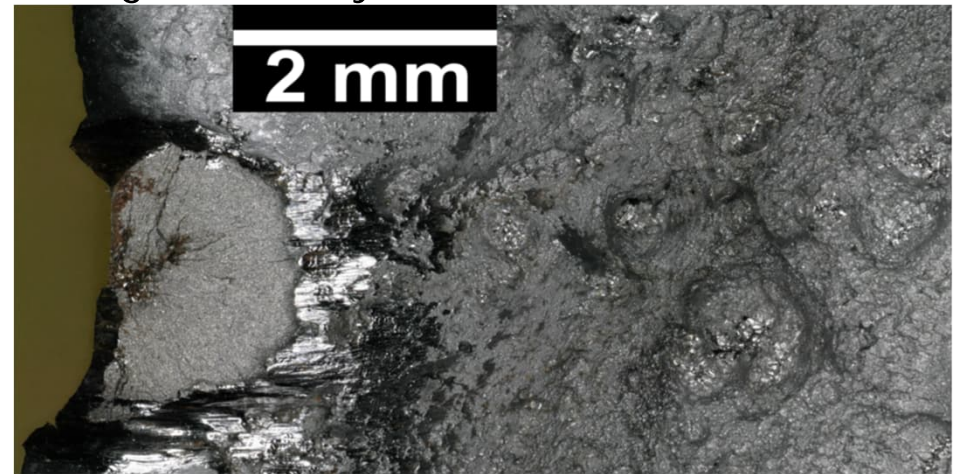
Cope



Blue arrow points to opened up secondary crack on machined surface opposite initiation side.



Machined surface opposite initiation side showing secondary crack



Zoom of opened-up secondary crack.

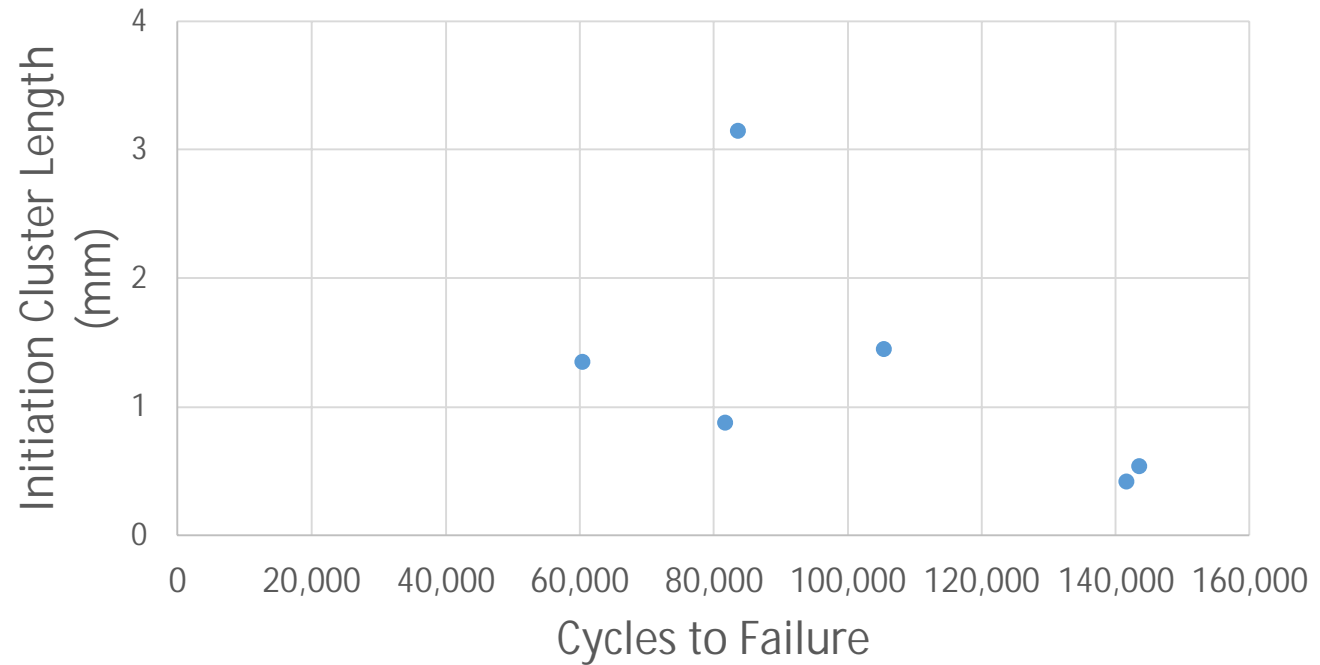
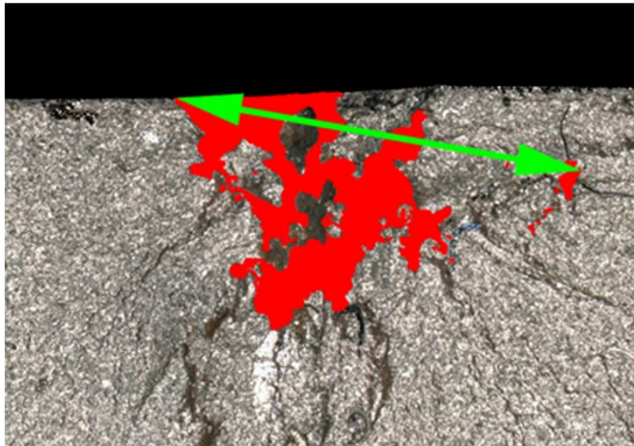
Measurements – Initiation Site

	Max Distance into Sample, mm	Initiation Area, mm ²	Initiation Cluster Size, mm	Cycles to Failure
100-1	2.09	1.46	3.15	83,594
100-2	0.31	0.04	0.42	141,655
100-3	0.88	0.44	1.35	60,446
114-1	0.86	0.10	0.88	81,734
114-2	0.46	0.09	0.54	143,511
114-3	0.67	0.27	1.45	105,374

Measurements Initiation and Secondary Cracks

Sample	Initiation Site	Secondary Crack 1		Secondary Crack 2		Secondary Crack 3		Total Crack Pore Area, Includes Initiation Site
	Initiation Area, mm ²	Initiation Area, mm ²	Initiation Cluster Size, mm	Initiation Area, mm ²	Initiation Cluster Size, mm	Initiation Area, mm ²	Initiation Cluster Size, mm	
100-1	1.46	2.33	3.02	2.64	3.56	0.38	1.37	6.82
100-2	0.04							0.04
100-3	0.44	2.48	0.90					2.92
114-1*	0.17							0.17
114-2	0.09							0.09
114-3	0.27	7.84	6.82	0.51	1.35	0.79	2.51	9.41

Cycles to Failure by Cluster Length



Pulstec μ -360s x-ray diffractometer (chromium tube)
Cosine α approach with area detector*
Sample surface is held horizontal so that incident angle of x-ray beam is controlled
X-Y positioning table is used to collect area scans or line scans

* Most XRD equipment instead uses \sin^2 theta approach

Rick Lopez
John Deere
Oct 2021

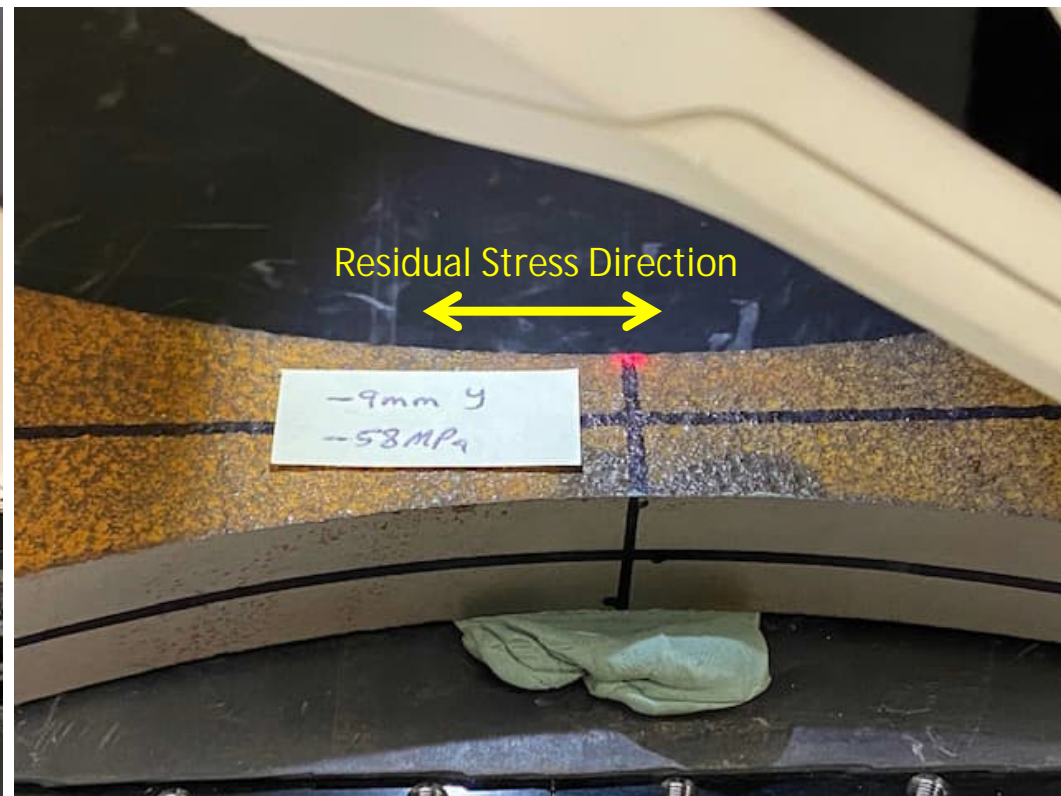
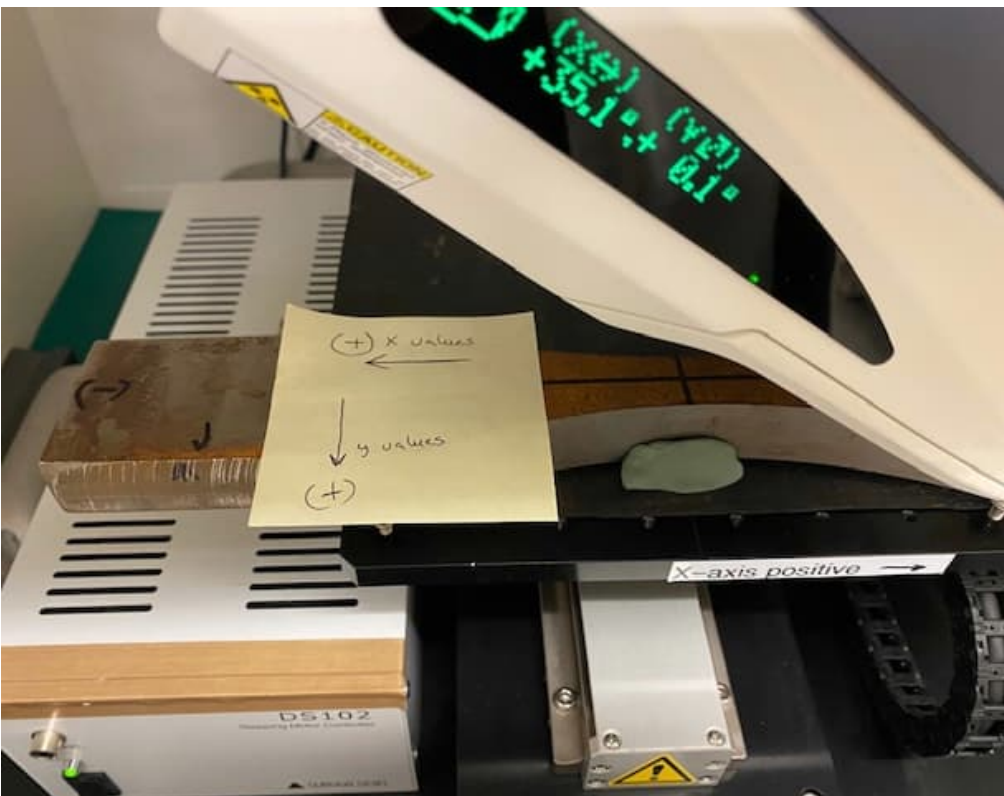


Public

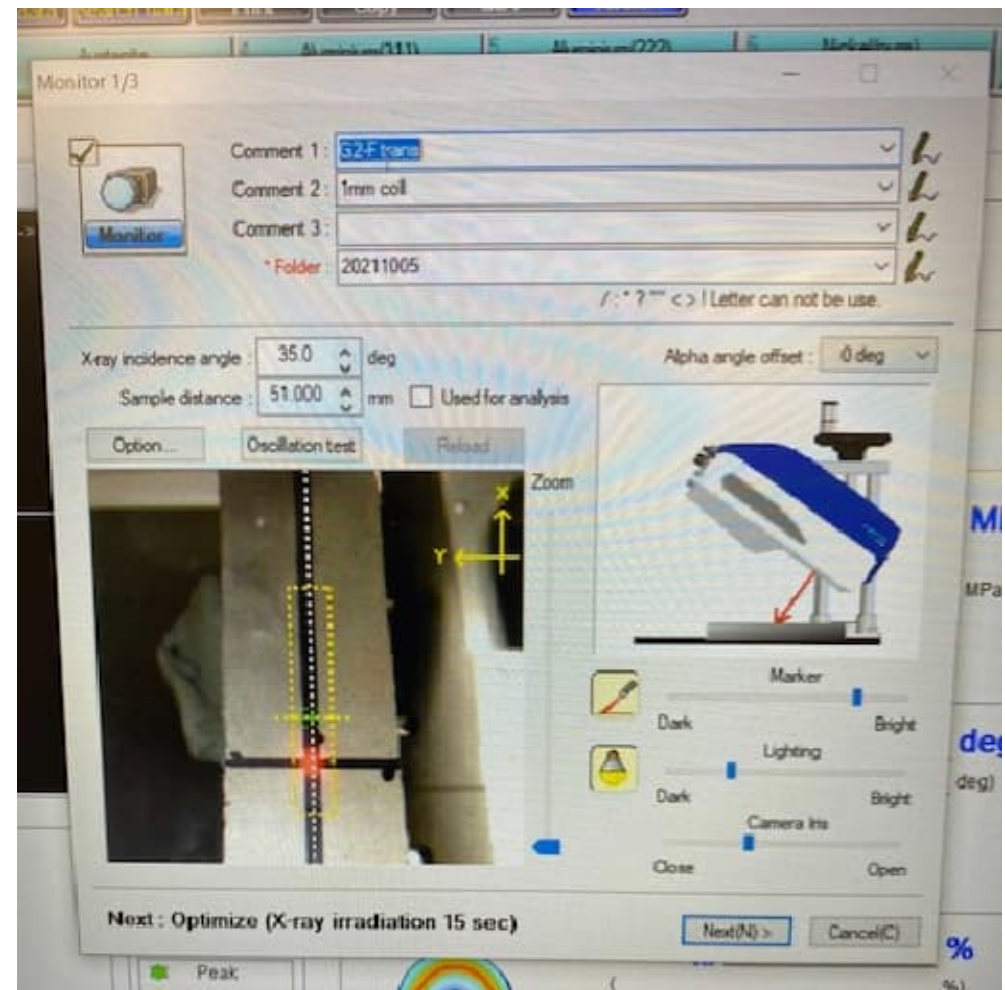
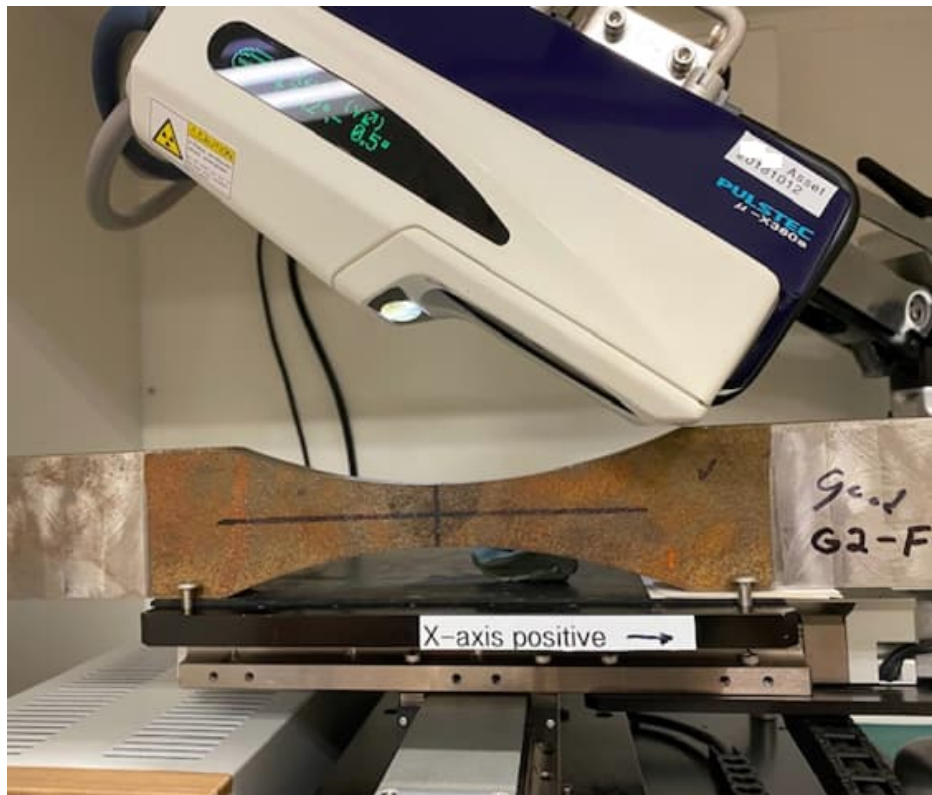
Location polarity within area and line scans is indicated below (left)

Example of typical value at a location is highlighted by laser dot (right)

Stress direction for all measurements was along the tensile testing longitudinal direction



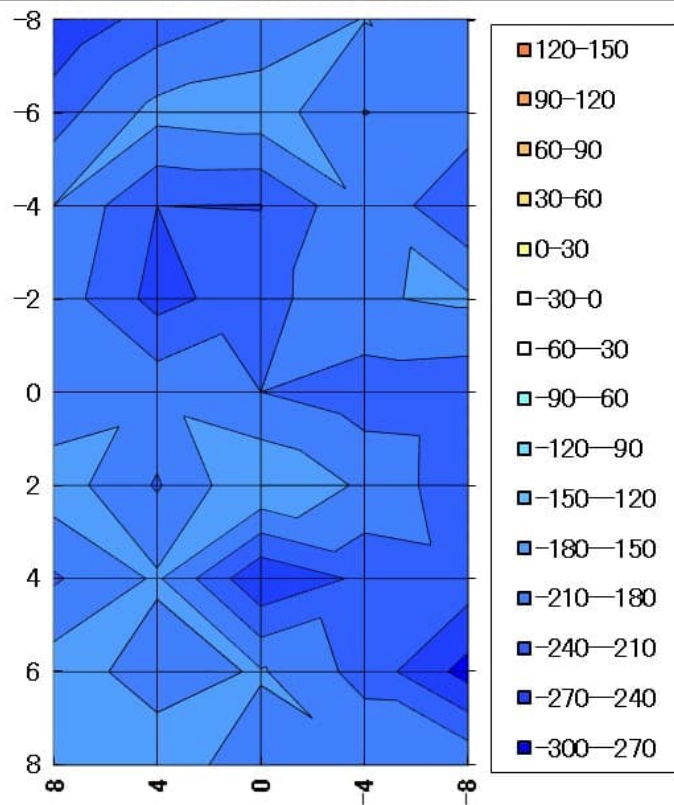
The measurement head was as close as possible to the sample for side locations
This caused sample distance to be slightly longer than preferred, but still allowable for valid data



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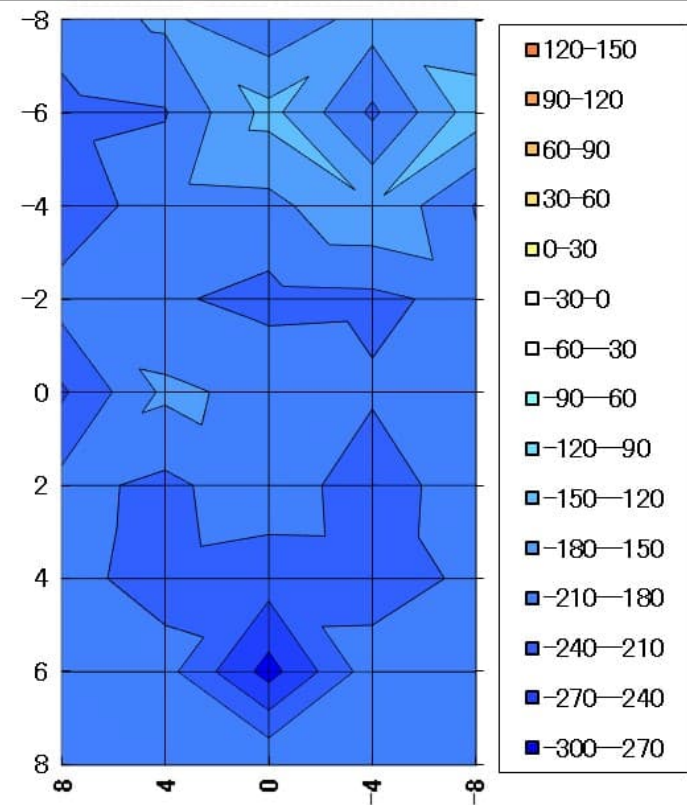
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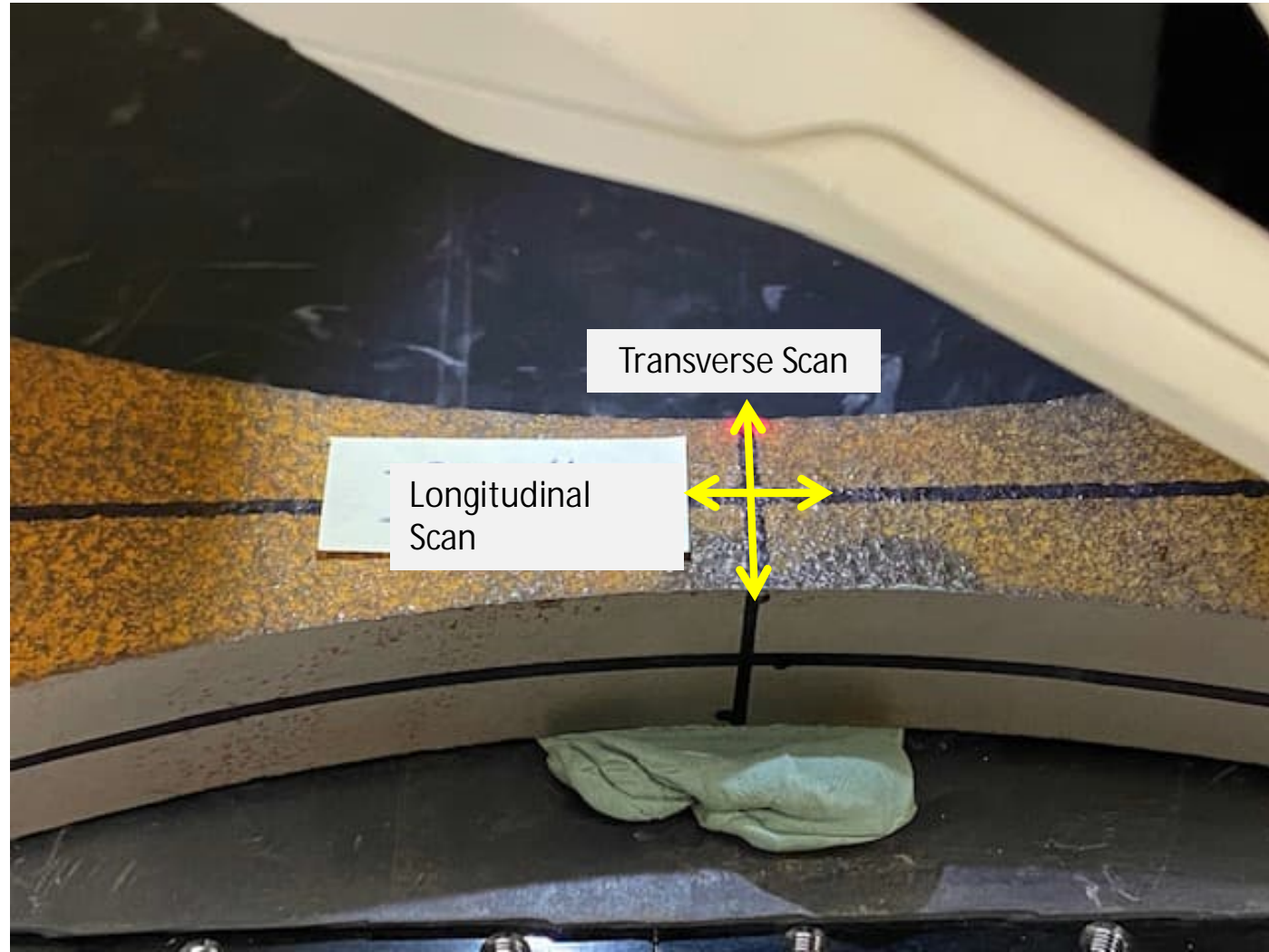


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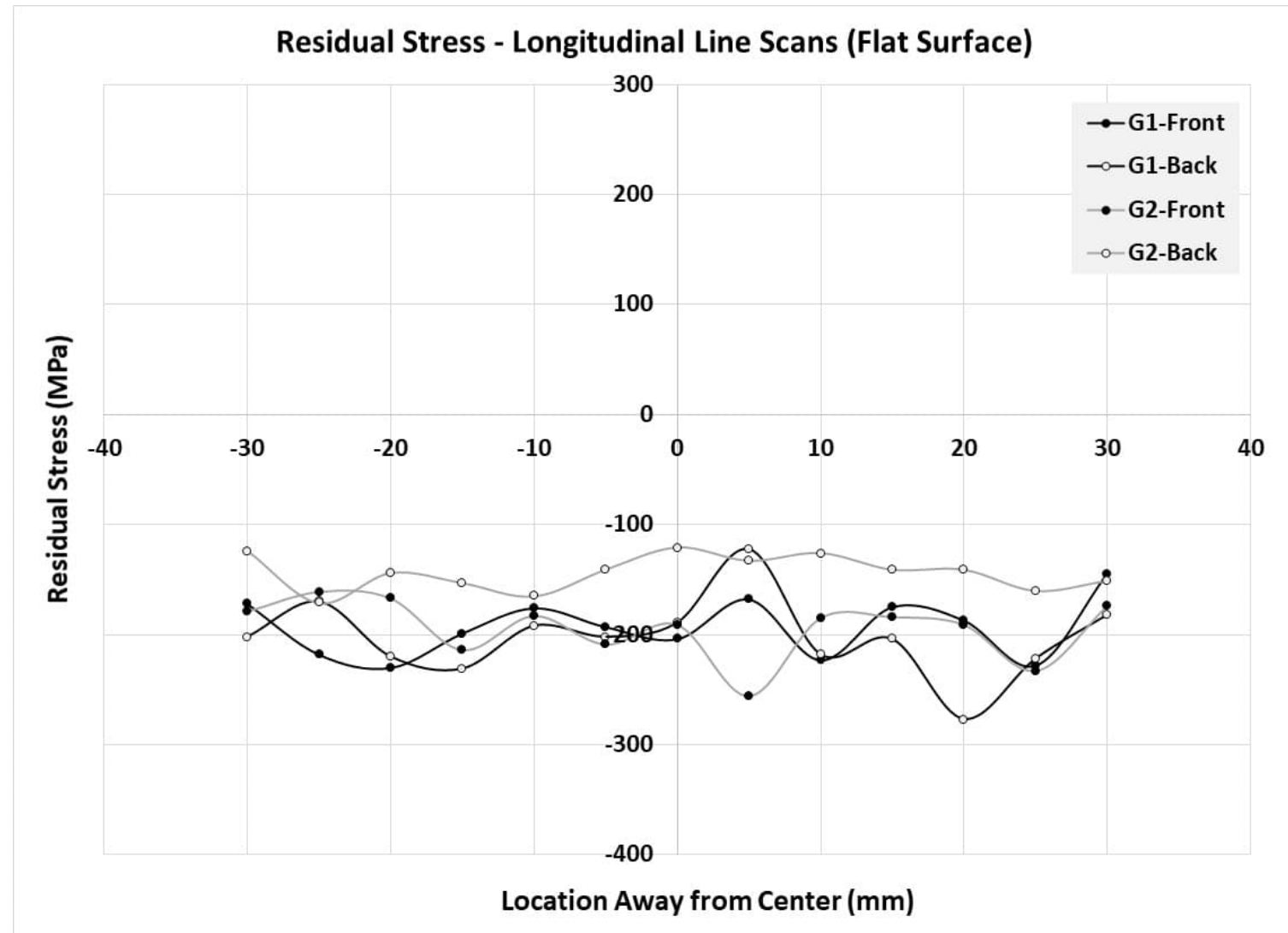
Max: -134 MPa





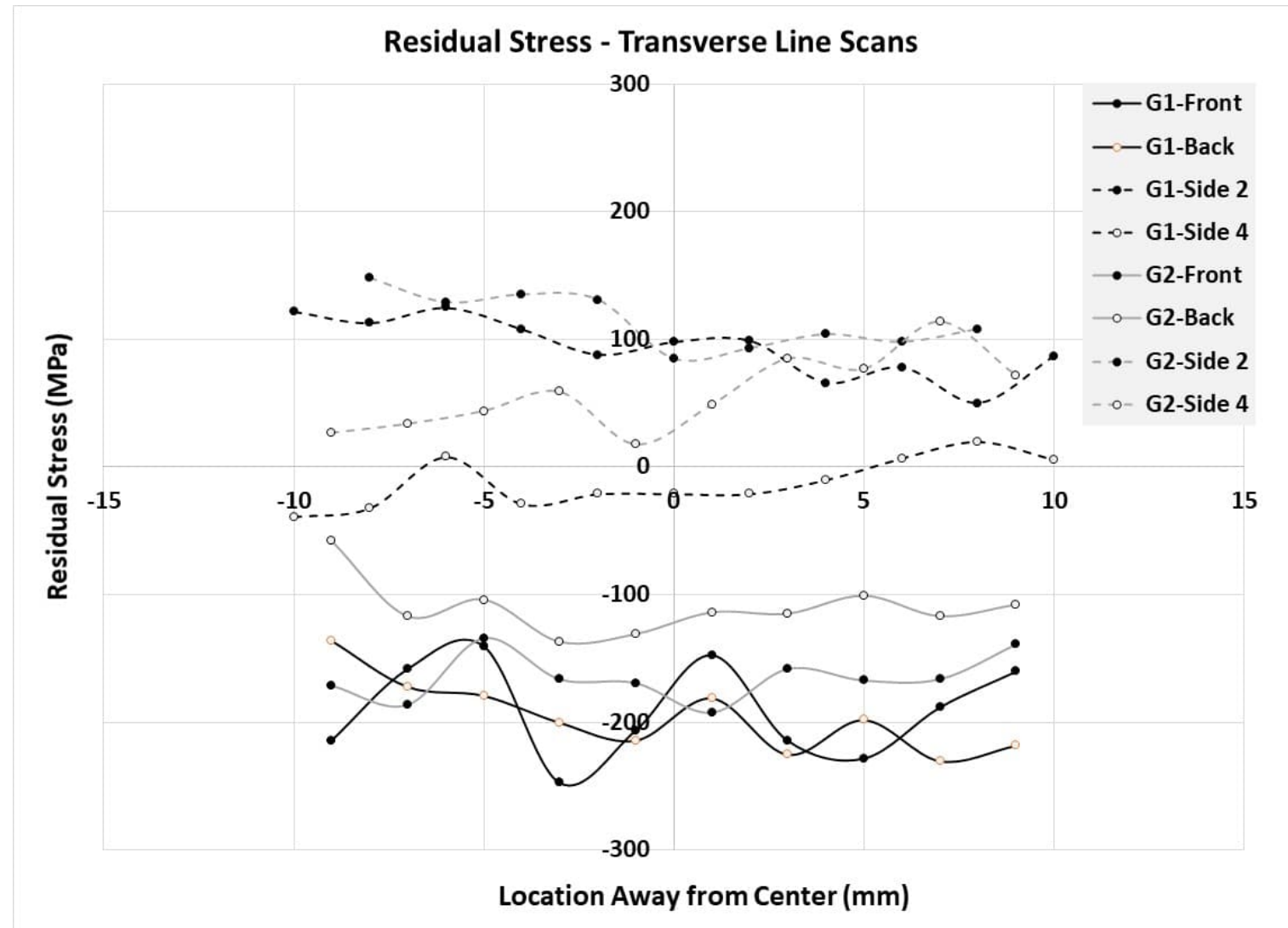
Longitudinal line scans, which were only possible on the flat as-cast surfaces

As-cast surfaces exhibited a lower (more compressive) residual stress. This is likely due to abrasive blast cleaning.

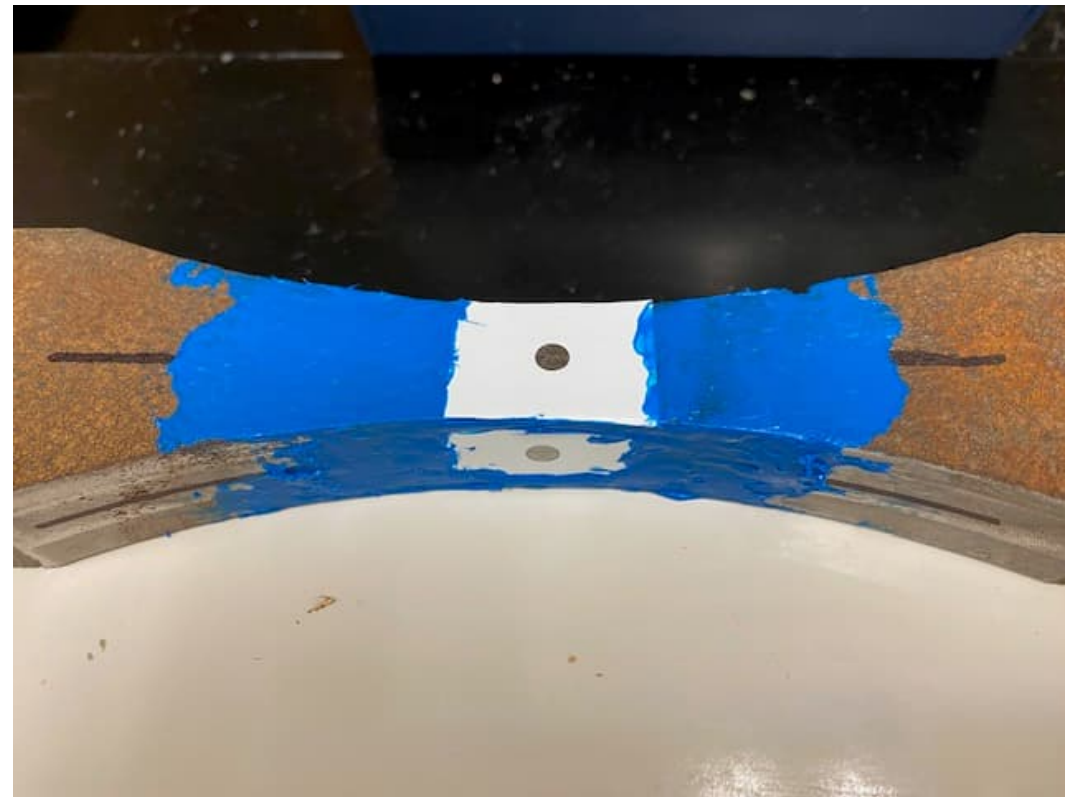


Transverse line scans, which were possible on all sides

Machined surfaces exhibited a higher (more tensile) residual stress



For one sample, a single location on the as-cast surface, and a single location on the water-jet cut and milled surface, was depth-profiled. A sticker mask with 5mm hole, and additional rubber masking, limited electropolishing to only this area. Depth measurements were taken with a physical depth gage, and measurements were quite variable initially on the as-cast surface (likely error).

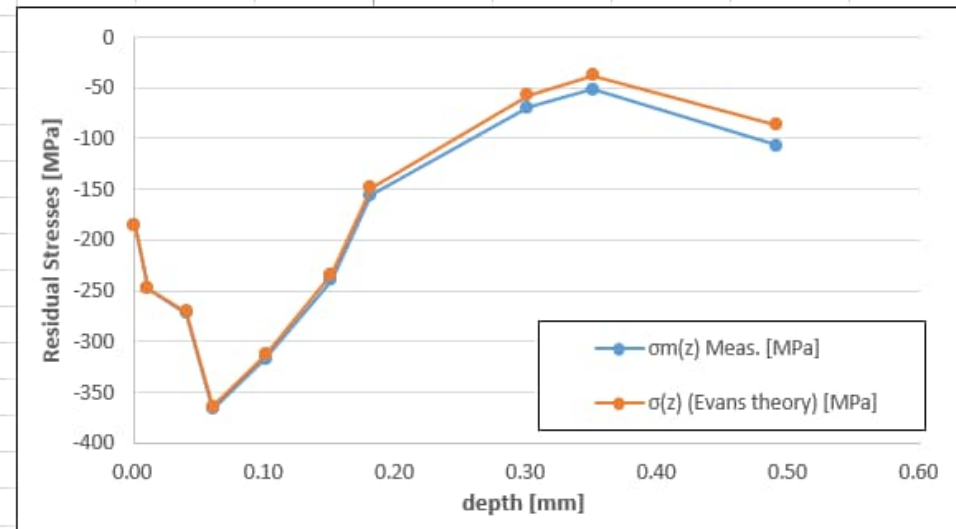
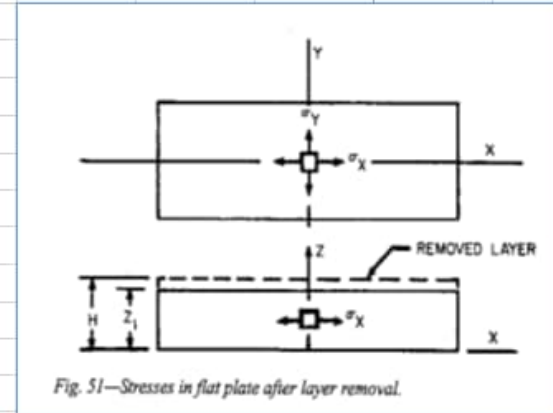


G3-Front (As-Cast Surface): Depth Profile Data After SAE HS-784 Flat Plate Correction

Material Removal Correction - FLAT PLATE

H [mm]	$\sigma_m(H)$ [MPa]
18	-185

Δz depth [mm]	$\sigma_m(z)$ Meas. [MPa]	$\sigma(z)$ (Evans theory) [MPa]
0.00	-185	-185.0
0.01	-248	-247.6
0.04	-272	-270.4
0.06	-367	-364.5
0.10	-317	-312.9
0.15	-240	-233.8
0.18	-156	-148.6
0.30	-70	-57.7
0.35	-52	-37.6
0.49	-107	-86.9
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0



Compressive stress continued to increase in magnitude to a depth of ~60 microns. At deeper depths the compressive stress decreased in magnitude, but remained compressive (negative values) through all depths tested.

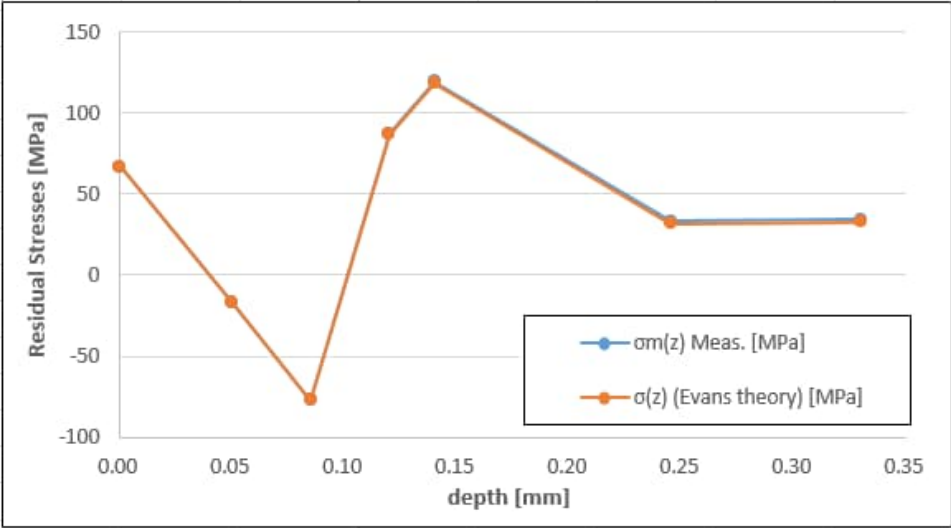
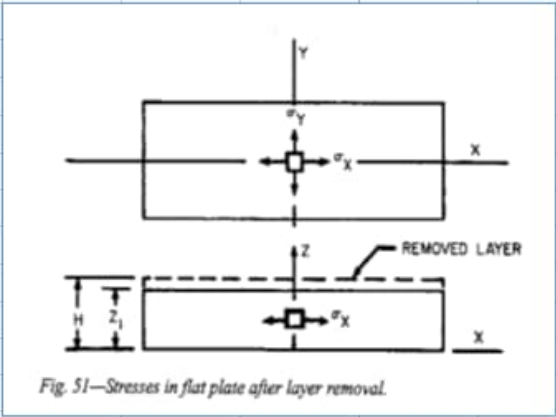
G3-Side (Water Jet + Milled): Depth Profile Data After SAE HS-784 Flat Plate Correction

Material Removal Correction - FLAT PLATE

H [mm]	$\sigma_m(H)$ [MPa]
60	67

Δz depth [mm]	$\sigma_m(z)$ Meas. [MPa]	$\sigma(z)$ (Evans theory) [MPa]
0.00	67	67.0
0.05	-17	-17.2
0.09	-77	-77.4
0.12	87	86.5
0.14	119	118.4
0.25	33	31.9
0.33	34	32.5
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0
		0.0

Tensile stress appeared to oscillate from tensile at the surface, to compressive (peaking at a depth of ~90 microns), and then tensile again at deeper depths.



Observations:

- As-cast surfaces exhibited longitudinal residual surface stresses as low as -282 MPa, and as high as -58 MPa.
- Water jet cut and milled surfaces exhibited longitudinal residual surface stresses as low as -39 MPa, and as high as +148 MPa.
- Depth profiles were performed on the as-cast and milled surfaces. These depth profiles were mathematically treated in a simple way to correct measurements for the relaxation due to removal of metal.